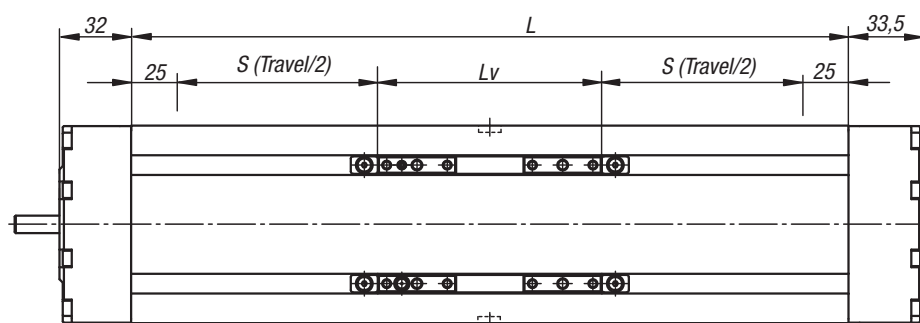


Technical information about linear actuators with ball screws

20331-10

Length calculation of the linear actuators

Size

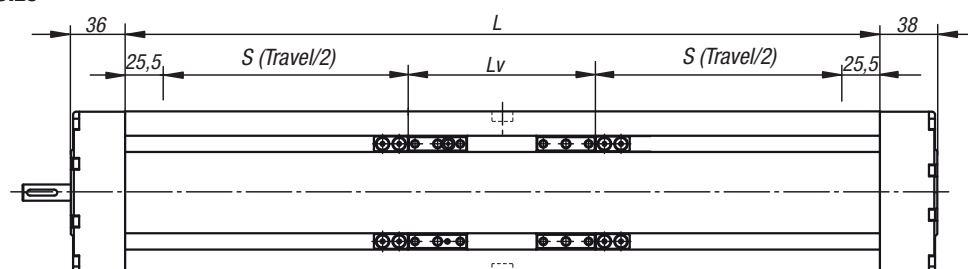


$$L = Strav + Lv + 50mm + 2 * travel\ reserve$$

$$L_{total} = L + 65,5mm$$

carriage	Length L_v
Form A	35
Form B	100

Size

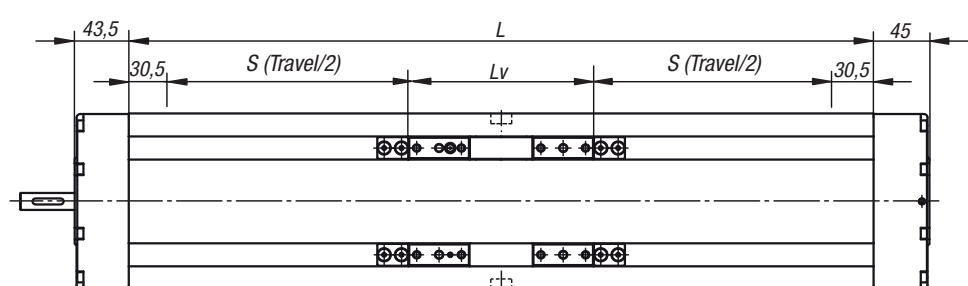


$$L = Strav + Lv + 51mm + 2 * travel\ reserve$$

$$L_{total} = L + 74mm$$

carriage	Length L_v
Form A	39
Form B	124

Size

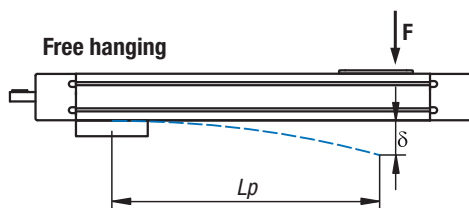
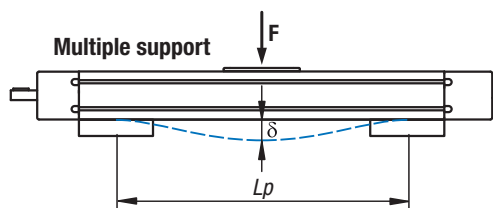


$$L = Strav + Lv + 61mm + 2 * travel\ reserve$$

$$L_{total} = L + 88.5mm$$

carriage	Length L_v
Form A	49
Form B	149

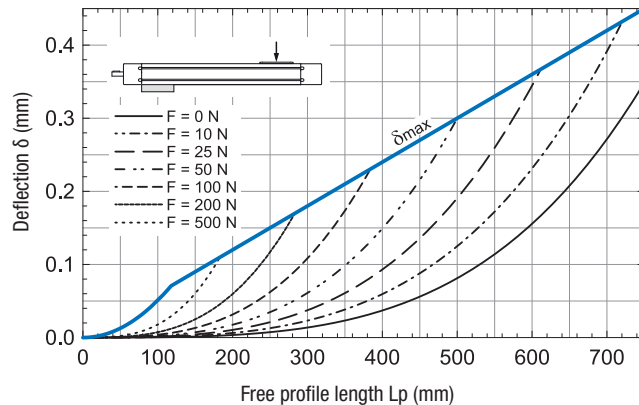
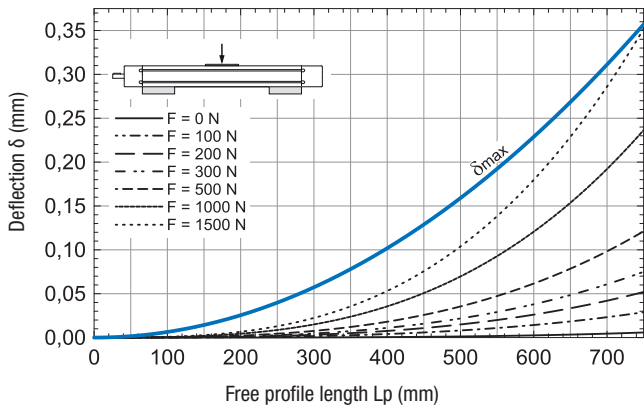
Deflection of the mechanical linear actuator



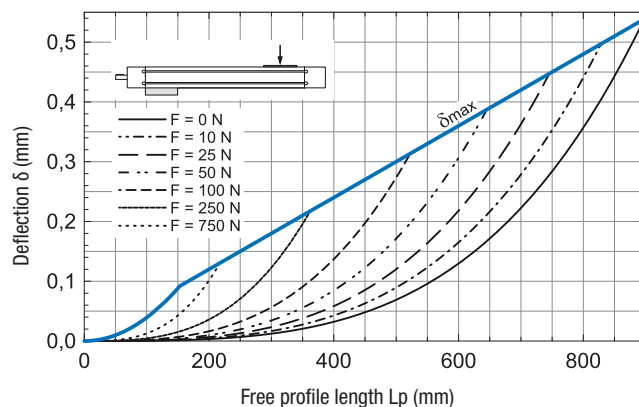
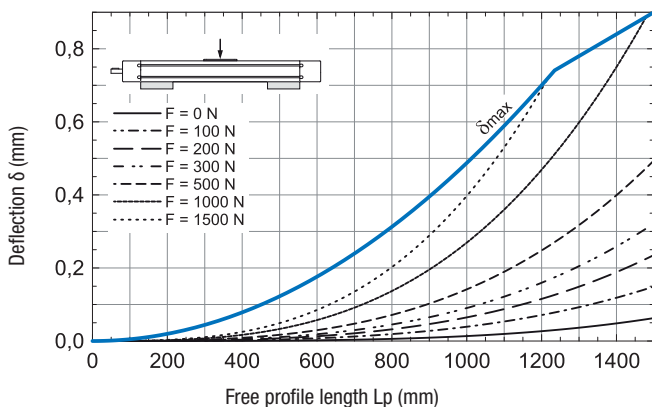
δ Maximum deflection of the linear actuator [mm]
 δ Maximum permissible deflection of the linear actuator [mm]
 F Force [N]
 L_p Free profile length [mm]

If the maximum deflection exceeds the permissible deflection, additional supports are required

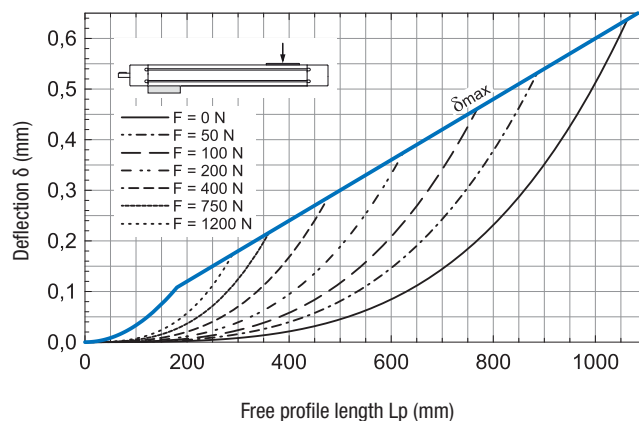
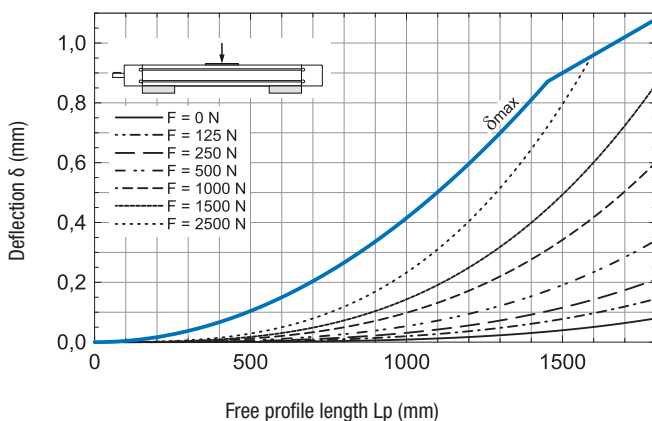
Size



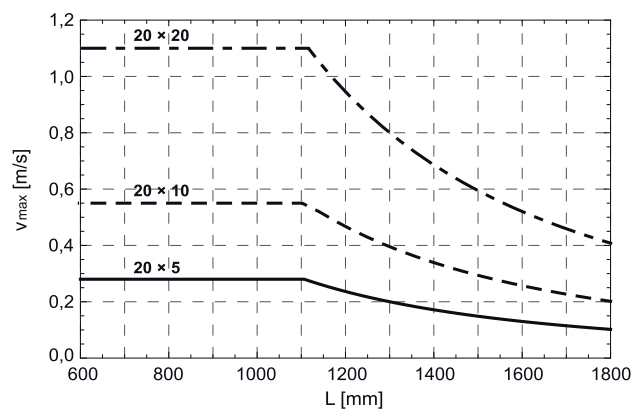
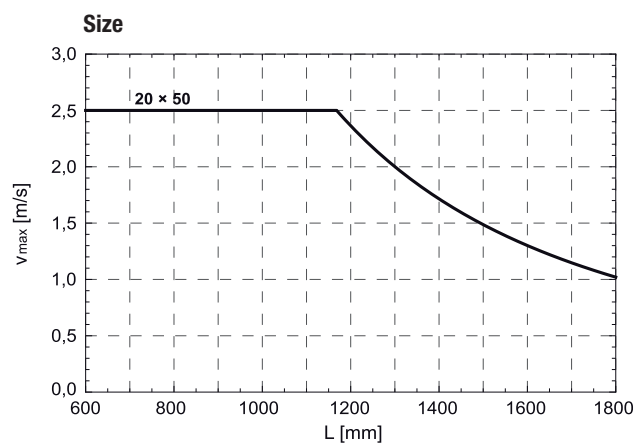
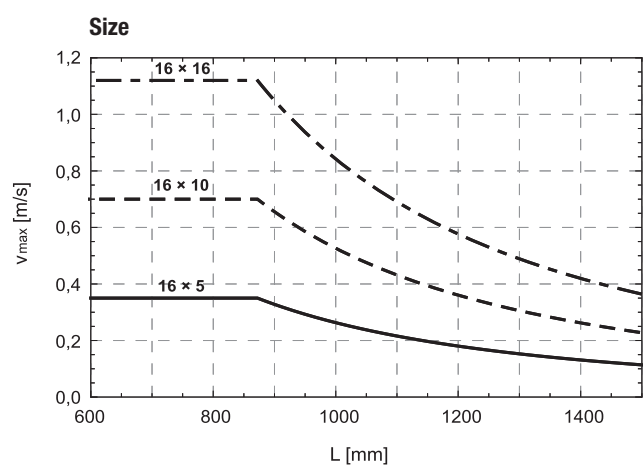
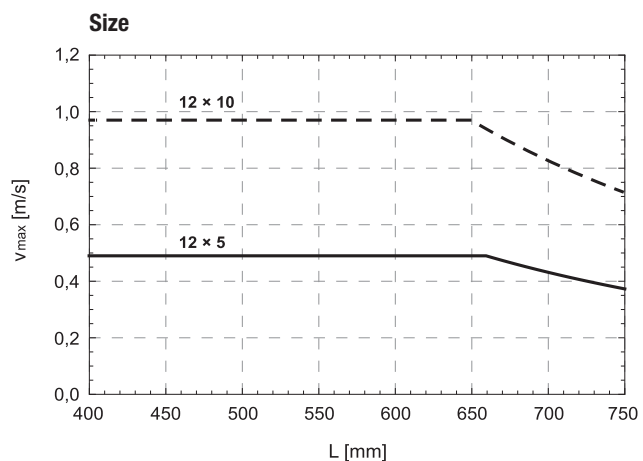
Size



Size



Maximum speed as a function of the profile length

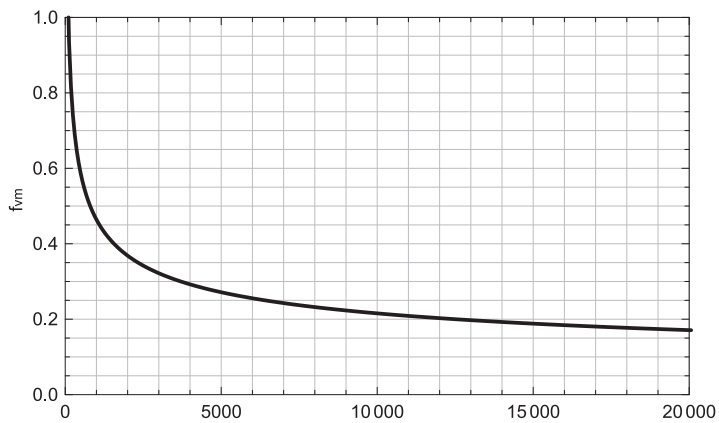


Weight and moment of inertia

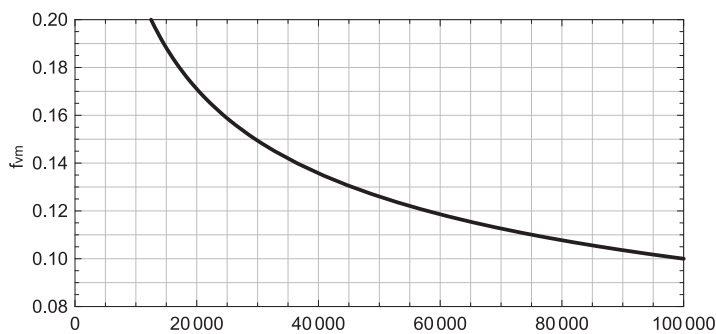
Size	Ball screw spindle DxT	carriage	Linear actuator weight kg	Moment of inertia 10-5 kg m ²
90	12x5	Form A	$1,6 + 0,006 * S \text{ Strav} + 0,30$	$0,32 + 0,002 * S \text{ Strav} + 0,02$
		Form B	$2,2 + 0,006 * S \text{ Strav} + 0,50$	$0,43 + 0,002 * S \text{ Strav} + 0,03$
	12x10	Form A	$1,6 + 0,006 * S \text{ Strav} + 0,30$	$0,38 + 0,002 * S \text{ Strav} + 0,08$
		Form B	$2,2 + 0,006 * S \text{ Strav} + 0,50$	$0,53 + 0,002 * S \text{ Strav} + 0,13$
110	16x5	Form A	$3,3 + 0,008 * S \text{ Strav} + 0,63$	$0,70 + 0,005 * S \text{ Strav} + 0,04$
		Form B	$4,6 + 0,008 * S \text{ Strav} + 1,36$	$1,19 + 0,005 * S \text{ Strav} + 0,09$
	16x10	Form A	$3,3 + 0,008 * S \text{ Strav} + 0,63$	$0,82 + 0,005 * S \text{ Strav} + 0,16$
		Form B	$4,6 + 0,008 * S \text{ Strav} + 1,36$	$1,45 + 0,005 * S \text{ Strav} + 0,34$
	16x16	Form A	$3,3 + 0,008 * S \text{ Strav} + 0,63$	$1,07 + 0,005 * S \text{ Strav} + 0,41$
		Form B	$4,6 + 0,008 * S \text{ Strav} + 1,36$	$1,99 + 0,005 * S \text{ Strav} + 0,88$
145	20x5	Form A	$5,7 + 0,015 * S \text{ Strav} + 1,19$	$3,04 + 0,013 * S \text{ Strav} + 0,08$
		Form B	$8,4 + 0,015 * S \text{ Strav} + 2,61$	$4,43 + 0,013 * S \text{ Strav} + 0,17$
	20x10	Form A	$5,7 + 0,015 * S \text{ Strav} + 1,19$	$3,27 + 0,013 * S \text{ Strav} + 0,30$
		Form B	$8,4 + 0,015 * S \text{ Strav} + 2,61$	$4,92 + 0,013 * S \text{ Strav} + 0,66$
	20x20	Form A	$5,7 + 0,015 * S \text{ Strav} + 1,19$	$4,17 + 0,013 * S \text{ Strav} + 1,21$
		Form B	$8,4 + 0,015 * S \text{ Strav} + 2,61$	$6,91 + 0,013 * S \text{ Strav} + 2,64$
	20x50	Form A	$5,7 + 0,015 * S \text{ Strav} + 1,19$	$10,50 + 0,013 * S \text{ Strav} + 7,54$
		Form B	$8,4 + 0,015 * S \text{ Strav} + 2,61$	$20,79 + 0,013 * S \text{ Strav} + 16,53$

Linear rails service life:

Comparison factor of the average load f_{vm} as a function of the service life L_{km}



More detailed view:



$$f_v = \frac{|F_y|}{C_{dyn}} + \frac{|F_z|}{C_{dyn}} + \frac{|M_x|}{M_{x\ dyn}} + \frac{|M_y|}{M_{y\ dyn}} + \frac{|M_z|}{M_{z\ dyn}}$$

f_v Load comparison factor

C_{dyn} Dynamic load rating

$M_{x\ dyn}$ Dynamic torque around the X axis Nm

$M_{y\ dyn}$ Dynamic torque around the Y axis Nm

$M_{z\ dyn}$ Dynamic torque around the Z axis Nm

F_y Acting force in Y axis N

F_z Acting force in Z axis N

M_x Effective torque around the X axis Nm

M_y Effective torque around the Y axis Nm

M_z Effective torque around the Z axis Nm

Calculation of the mean load comparison factor f_{vm} :

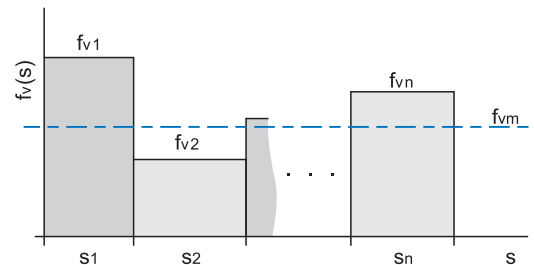
$$f_{vm} = \sqrt[3]{\frac{f_{v1}^3 \times s_1 + f_{v2}^3 \times s_2 + \dots + f_{vn}^3 \times s_n}{s_1 + s_2 + \dots + s_n}}$$

f_{vm} Mean load comparison factor

f_v i-th load comparison factor of a given load mode $f_v(s)$, $i \in [1, 2, \dots, n]$

s_i i-th travel of a given load mode $f_v(s)$, $i \in [1, 2, \dots, n]$

Load mode $f_v(s)$



Calculation of the service life:

$$L_{km} = \left(\frac{1}{f_{vm}} \right)^3 \cdot 10^2$$

L_{km} Service life (km)

Safety factor f_s :

$$f_s = \frac{1}{f_{vm}}$$

The safety factor depends on the application and its required safety. We recommend a minimum safety factor $f_s = 5.0$.

f_s Safety factor

Permissible load factor f_p for linear guide

$$f_p = \frac{|F_y|}{F_{py}} + \frac{|F_z|}{F_{pz}} + \frac{|M_x|}{M_{px}} + \frac{|M_y|}{M_{py}} + \frac{|M_z|}{M_{pz}} \leq 1$$

f_p Permissible load factor

F_{py} Max. permissible force in Y axis N

F_{pz} Max. permissible force in Z axis N

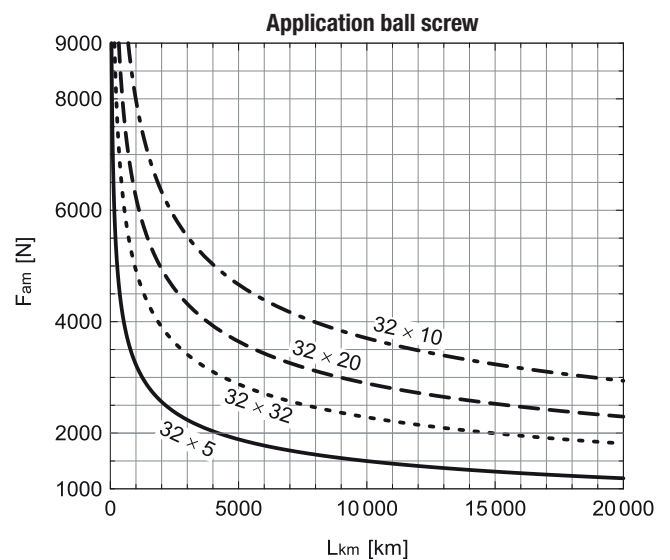
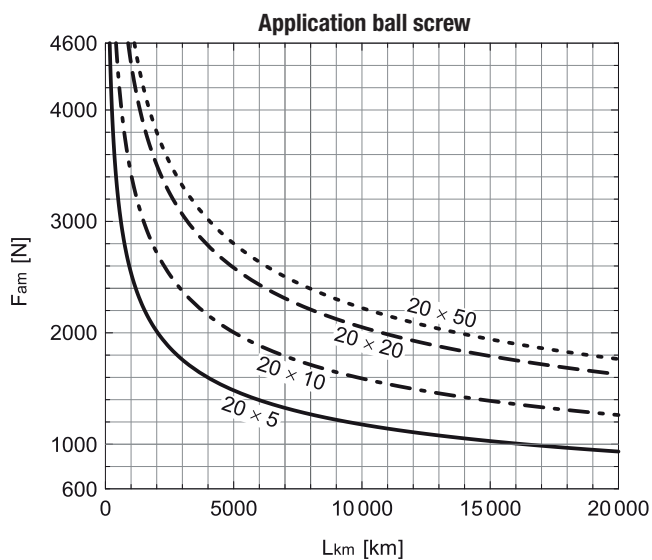
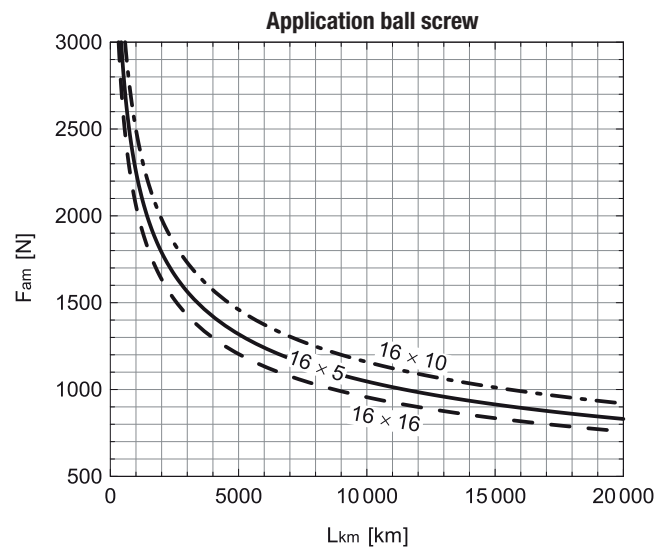
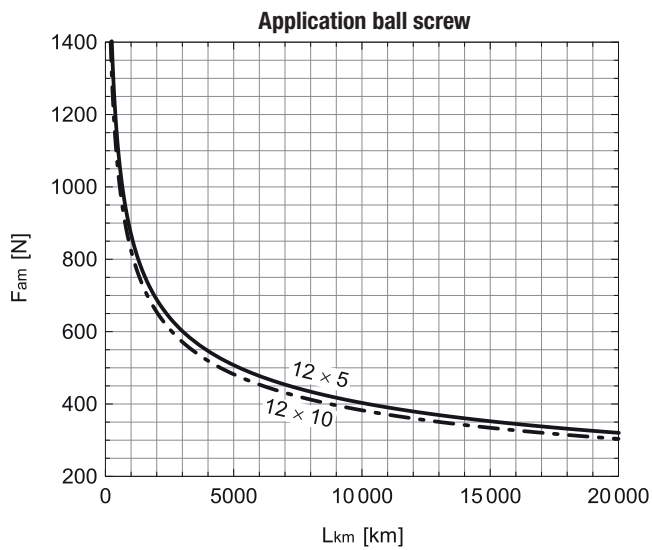
M_{px} Max. permissible torque around the X axis Nm

M_{py} Max. permissible torque around the Y axis Nm

M_{pz} Max. permissible torque around the Z axis Nm

Ball screw service life

Applied average axial force F_{am} as a function of service life L_{km}



The diagrams show the theoretical service life for the ball screw when the average axial force F_{am} is taken into account.

Calculation of the mean axial force F_{am}

$$F_{am} = \sqrt[3]{\frac{|F_{a1}|^3 \times s_1 + |F_{a2}|^3 \times s_2 + \dots + |F_{an}|^3 \times s_n}{s_1 + s_2 + \dots + s_n}}$$

F_{am} mean axial force

F_{ai} i-te axial force of a given load mode $F_a(s)$, $i \in [1, 2, \dots, n]$

s_i i-te travel of a given load mode $F_a(s)$, $i \in [1, 2, \dots, n]$

Load mode $F_a(s)$

